

Numerical Methods

Lecture 3: Perturbation Methods

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Traditional Methods

- Before large-scale computing resources available, economists made do with what they had
- Popular method: Linearizing/log-linearizing
- Idea
 1. Boil complicated non-linear relationships down to something tractable
 2. Use linear algebra (requires little numerical power)
- Log-linearizing
 1. Often yields easier solution than linearizing
 2. Gets rid of units; can talk about %-changes
 3. Not quite right...
 - Economists eventually started accepting the log-linearized model as the relevant model instead of the full, microfounded one

Log-Linearizing

- 'Oldest' trick in the books
- A bit ad-hoc when it was first implemented; more sophisticated techniques developed
- Basic idea
 1. Take log of all equilibrium conditions
 2. Linearize (Taylor-expand) system around a point (steady state)
 3. Manipulate until all variables of interest are percentage deviations

Why?

- Suppose we have a nonlinear relationship

$$f(x) = \frac{g(x)h(x)}{\eta(x)}$$

- Taking logs yields

$$\log f(x) = \log g(x) + \log h(x) - \log \eta(x)$$

- Piecewise (bit-by-bit) first-order approximation around \bar{x}

$$\log f(\bar{x}) + \frac{f'(\bar{x})}{f(\bar{x})}[x - \bar{x}] \approx \log g(\bar{x}) + \frac{g'(\bar{x})}{g(\bar{x})}[x - \bar{x}] + \dots$$

Why?

- Notice that the constant terms all cancel. Divide remaining expressions by \bar{x} ...

$$\frac{f'(\bar{x})}{f(\bar{x})} \hat{x} \approx \frac{g'(\bar{x})}{g(\bar{x})} \hat{x} + \frac{h'(\bar{x})}{h(\bar{x})} \hat{x} - \frac{\eta'(\bar{x})}{\eta(\bar{x})} \hat{x}$$

where $\hat{x} = \frac{x-\bar{x}}{\bar{x}}$ i.e. percent deviation of x from steady state

- Linear in \hat{x} . Impose equality to approximate the system
- Notice that \hat{x} is approximated around zero by construction

Additive/Multivariate Systems

- What if $y_t = g(x_t) + z_t$?

$$\implies \log y_t = \log(g(x_t) + z_t)$$

$$\log(\bar{y}) + \frac{1}{\bar{y}}[y_t - \bar{y}] = \log(g(\bar{x}) + \bar{z}) + \frac{g'(\bar{x})[x_t - \bar{x}] + [z_t - \bar{z}]}{g(\bar{x}) + \bar{z}}$$

- Exploit $\bar{y} = g(\bar{x}) + \bar{z}$

$$\frac{1}{\bar{y}}[y_t - \bar{y}] = \frac{g'(\bar{x})}{\bar{y}}[x_t - \bar{x}] + \frac{1}{\bar{y}}[z_t - \bar{z}]$$

- Cannot divide whole thing by \bar{x} . Multiply and divide each term by SS component

$$\hat{y}_t = \frac{\bar{x}g'(\bar{x})}{\bar{y}}\hat{x}_t + \frac{\bar{z}}{\bar{y}}\hat{z}_t$$

Example: NCG Model, CRRA-utility

- Two-variable dynamical system

$$c_t^{-\sigma} = \beta(\alpha k_{t+1}^{\alpha-1} + 1 - \delta)c_{t+1}^{-\sigma}$$

$$c_t + k_{t+1} = k_t^\alpha + (1 - \delta)k_t$$

- Example worked out on board in class
- Notice why it's ad hoc: Technically the log β term should go away...Doesn't happen when we do it 'bit-by-bit'

$$\hat{k}_{t+1} = [\alpha \bar{k}^{\alpha-1} + 1 - \delta]\hat{k}_t - \frac{\bar{c}}{\bar{k}}\hat{c}_t$$

$$\hat{c}_{t+1} = \hat{c}_t + \frac{\alpha(\alpha-1)\bar{k}^\alpha}{\sigma[\alpha\bar{k}^{\alpha-1} + 1 - \delta]}\hat{k}_{t+1}$$

Stability I

- Want our approximation to be stationary around zero
- Express linear dynamical system as

$$\hat{x}_{t+1} = A\hat{x}_t$$

for a matrix A

- Here, $\hat{x}_t = [k_t, c_t]'$ and

$$A = \begin{bmatrix} [\alpha \bar{k}^{\alpha-1} + 1 - \delta] & -\frac{\bar{c}}{\bar{k}} \\ \frac{\alpha(\alpha-1)\bar{k}^\alpha}{\sigma} & 1 - \frac{\alpha(\alpha-1)\bar{k}^\alpha}{\sigma[\alpha\bar{k}^{\alpha-1} + 1 - \delta]} \frac{\bar{c}}{\bar{k}} \end{bmatrix}$$

Substituted in RC to get \hat{k}_{t+1} out of Euler Equation

Stability II

- Intuitively, it will be stable if we start from some \hat{x}_t 'near' zero and it goes to zero over time i.e.

$$\lim_{n \rightarrow \infty} A^n \hat{x}_t = \mathbf{0}$$

- Think back to eigenvalues

$$Av = \gamma v$$

for some eigenvalue, γ , and eigenvector v

- If eigenvalues are distinct, then so are eigenvectors
 - \implies Eigenvectors can span 2D-space

Stability III

- Since eigenvectors span the space, we can write any \hat{x}_t as a combination of the eigenvalues

$$\hat{x}_t = \alpha_{1,t}\nu_1 + \alpha_{2,t}\nu_2$$

for some constants $\alpha_{1,t}$ and $\alpha_{2,t}$

- Now

$$\begin{aligned}\lim_{n \rightarrow \infty} A^n \hat{x}_t &= \lim_{n \rightarrow \infty} A^n [\alpha_{1,t}\nu_1 + \alpha_{2,t}\nu_2] \\ &= \alpha_{1,t} \lim_{n \rightarrow \infty} A^n \nu_1 + \alpha_{2,t} \lim_{n \rightarrow \infty} A^n \nu_2 \\ &= \alpha_{1,t} \lim_{n \rightarrow \infty} \gamma_1^n \nu_1 + \alpha_{2,t} \lim_{n \rightarrow \infty} \gamma_2^n \nu_2\end{aligned}$$

Stability IV

- 3 possible cases
 1. $|\gamma_1|, |\gamma_2| < 1$ i.e. globally stable
 2. $|\gamma_1|, |\gamma_2| \geq 1$ i.e. globally unstable
 3. $|\gamma_i| < 1$ and $|\gamma_j| \geq 1$ i.e. saddle-path stable
- NCG model falls is saddle-path stable (one-dimensional stable manifold)
 - Given a k_t , only one c_t will work
 - Will be a c_t such that \hat{x}_t implies $\alpha_{j,t} = 0$
 - i.e. in span of stable eigenvector (easy to compute)
- Sidenote: If γ_i is complex, solution 'spirals' toward/away from steady state

Adding Shocks

- The RBC model has a random component. RC deterministic, but EE given by

$$c_t^{-\sigma} = \beta E_t [(\alpha e^{z_{t+1}} k_{t+1}^{\alpha-1} + 1 - \delta) c_{t+1}^{-\sigma}]$$

- Taking logs

$$-\sigma \log c_t = \log \beta + \log E_t [(\alpha e^{z_{t+1}} k_{t+1}^{\alpha-1} + 1 - \delta) c_{t+1}^{-\sigma}]$$

but $\log(E[x]) \neq E[\log(x)]$...

- So people ignore this! (faux pas number two)
- Charge ahead and derive something like

$$-\sigma \hat{c}_t = -\sigma E_t \hat{c}_{t+1} + \gamma_1 \hat{k}_{t+1} + \gamma_2 E_t z_{t+1}$$

where γ_1 and γ_2 are known combinations of parameters

LRE Models

- But even here is a problem:
 - Want something like

$$\begin{bmatrix} k_t \\ c_t \\ z_t \end{bmatrix} = A \begin{bmatrix} k_{t-1} \\ c_{t-1} \\ z_{t-1} \end{bmatrix} + B\epsilon_t$$

- How to get rid of $E_t[c_{t+1}]$ terms?
- These models are often called **Linear Rational Expectations Models**
 - Sims (2002) proposed most common solution

LRE Solution: Applicability

- Designed for models of form

$$\Gamma_0 y_t = \Gamma_1 y_{t-1} + C + \Psi z_t + \Pi \eta_t$$

- Some elements of y_t are expectations of future elements

$$x_t = E_{t-1}[x_t] + \eta_t$$

1. States (including expected states): $y_t = [x_t, E_t x_{t+1}]'$
2. Vector of constants: C
3. Exogenous shock processes: z_t
4. Expectations errors: η_t (not exogenous; part of solution)

Procedure

- Assume either
 1. $\Gamma_0 = I_n$
 2. Γ_0 non-singular; pre-multiply everything through by it
- Work with system (with possible redefinition of RHS matrices)

$$y_t = \Gamma_1 y_{t-1} + C + \Psi z_t + \Pi \eta_t$$

- **Step 1:** Jordan Decomposition of Square Matrix

$$\Gamma_1 = P \Lambda P^{-1}$$

1. P : Matrix of (generalized) eigenvectors of Γ_1
2. Λ : Diagonal matrix of eigenvalues
 - Place 2 identical eigenvalues next to each other
 - $\Lambda_{i,i+1} = 1$ if $\Lambda_{i,i} = \Lambda_{i+1,i+1}$

Procedure

- **Step 2:** Pre-multiply by P^{-1}

- Define $w_t = P^{-1}y_t$

$$w_t = \Lambda w_{t-1} + P^{-1}C + P^{-1}(\Psi z_t + \Pi \eta_t)$$

- This system breaks into completely independent 'blocks' by eigenvalue, with a typical block

$$w_{j,t} = \begin{bmatrix} \lambda_j & 1 & 0 & \dots & 0 \\ 0 & \lambda_j & 1 & \dots & 0 \\ 0 & 0 & \dots & \dots & 0 \\ \dots & \dots & \dots & \lambda_j & 1 \\ 0 & \dots & 0 & 0 & \lambda_j \end{bmatrix} w_{j,t-1} + P^{j\cdot} C + P^{j\cdot} (\Psi z_t + \Pi \eta_t)$$

where $P^{j\cdot}$ is matrix of corresponding rows of P^{-1}

Procedure

- Steady state solution will impose z_t and η_t equal zero

$$w_{j,t} = [I - \Lambda_j]^{-1} P^j \cdot C$$

- Notice a block-system is stationary iff $|\lambda_j| < 1$
- **Step 3:** Separate blocks into two groups: S (stable) and U (unstable)
 - In any solution, it must be the case that

$$w_{U,t} = [I - \Lambda_U]^{-1} P^U \cdot C$$

for *all* t (otherwise it would explode)

- Implies shocks must satisfy (for any t)

$$P^U \cdot (\Psi z_t + \Pi \eta_t) = 0$$

Procedure

- For a solution to exist, it must be that

$$\text{span}(P^U \cdot \Psi) \subset \text{span}(P^U \cdot \Pi)$$

i.e. expectations shocks can always arise to offset exogenous shocks in unstable manifold (keeping it in steady state)

- For a solution to be unique, it must be that

$$\text{span}(\Pi'(P^S \cdot)') \subset \text{span}(\Pi'(P^U \cdot)')$$

i.e. there must be only *one* such set of expectations shocks

- **Step 5:** If these conditions hold, then a matrix Φ exists such that

$$P^S \cdot \Pi \eta = \Phi P^U \cdot \Pi \eta$$

Procedure

- To solve for Φ ...
- Run a 'regression' of $P^{U \cdot} \Pi$ on $P^{S \cdot} \Pi$
 - Residuals should be zero since it's in the span
- $y = X\beta \implies \beta = (X'X)^{-1}X'y$
 1. $\beta = \Phi'$
 2. $X = \Pi'(P^{U \cdot})'$
 3. $y = \Pi'(P^{S \cdot})'$
$$\Phi' = [P^{U \cdot} \Pi \Pi'(P^{U \cdot})']^{-1} P^{U \cdot} \Pi \Pi'(P^{S \cdot})'$$
- If $X'X$ is singular, either
 1. No solution exists
 2. Φ can be trivially found via inspection
- Often (2) is the case in simple, one-shock models

Procedure

- **Step 6:** Use Φ -matrix to get rid of expectation shocks

$$\begin{bmatrix} w_{S,t} \\ w_{U,t} \end{bmatrix} = \begin{bmatrix} \Lambda_S \\ 0 \end{bmatrix} w_{S,t-1} + \begin{bmatrix} P^S \cdot C \\ [I - \Lambda_U]^{-1} P^U \cdot C \end{bmatrix} + \begin{bmatrix} I & -\Phi \\ 0 & 0 \end{bmatrix} P^{-1} \Psi z_t$$

- Now use $y_t = P w_t$ to go back!

$$y_t = \Theta_1 y_{t-1} + \Theta_c C + \Theta_z z_t$$

1. $\Theta_1 = P \cdot_S \Lambda_S P^S \cdot$
 2. $\Theta_c = P \cdot_S P^S \cdot + P \cdot_U [I - \Lambda_U]^{-1} P^U \cdot$
 3. $\Theta_z = [P \cdot_S P^S \cdot - P \cdot_S \Phi P^U \cdot] \Psi$
- Expectation error shocks gone!

Application

- To completely characterize mapping from initial conditions and z , we need to initialize expectation terms i.e.

$$E_t y_{t+s} = \Theta_1^s y_t + (I - \Theta_1^{s+1})(I - \Theta_1)^{-1} \Theta_c C$$

- Can simulate model, analyze partial derivatives, etc.
- Impulse response functions can be computed in closed-form

$$y_{t+s} - E_t y_{t+s} = \sum_{\nu=0}^{s-1} \Theta_1^\nu \Theta_z z_{t+s-\nu}$$

Example: Stochastic NCG Model

- Log-linearized equations

$$\hat{k}_{t+1} = [\alpha \bar{k}^{\alpha-1} + 1 - \delta] \hat{k}_t + \bar{k}^\alpha z_t - \frac{\bar{c}}{\bar{k}} \hat{c}_t$$

$$-\sigma \hat{c}_t = -\sigma E_t \hat{c}_{t+1} + \left[\frac{\alpha(\alpha-1)\bar{k}^{\alpha-1}}{\alpha\bar{k}^{\alpha-1} + 1 - \delta} \right] \hat{k}_{t+1} + \left[\frac{\alpha\bar{k}^{\alpha-1}}{\alpha\bar{k}^{\alpha-1} + 1 - \delta} \right] \underbrace{E_t z_{t+1}}_{=\rho z_t}$$

- Substitute out \hat{k}_{t+1} into EE

$$\hat{k}_{t+1} = [\alpha \bar{k}^{\alpha-1} + 1 - \delta] \hat{k}_t + \bar{k}^\alpha z_t - \frac{\bar{c}}{\bar{k}} \hat{c}_t$$

$$\left[\frac{\alpha(\alpha-1)\bar{k}^{\alpha-1}}{\alpha\bar{k}^{\alpha-1} + 1 - \delta} \frac{\bar{c}}{\bar{k}} - \sigma \right] \hat{c}_t = -\sigma E_t \hat{c}_{t+1} + [\alpha(\alpha-1)\bar{k}^{\alpha-1}] \hat{k}_t + \left[\frac{\alpha(\alpha-1)\bar{k}^{2\alpha-1} + \rho\alpha\bar{k}^{\alpha-1}}{\alpha\bar{k}^{\alpha-1} + 1 - \delta} \right] z_t$$

Example: Stochastic NCG Model

1. $y_t = [\hat{k}_t, \hat{c}_t, E_t[\hat{c}_{t+1}], z_t]$
2. $z_t = \epsilon_t$ (from AR(1))
3. $C = 0$
4. $\hat{c}_t = E_{t-1}[\hat{c}_t] + \eta_t$
 - z_t term in Euler Equation: $z_t = \rho z_{t-1} + \sigma_z \epsilon_t$
 - Lag resource constraint
 - Substitute RC into Euler Equation to eliminate \hat{k}_{t+1}

Example: Stochastic NCG Model

$$\Gamma_0 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ -\frac{\alpha(\alpha-1)\bar{k}^{\alpha-1}}{\sigma} & \left[\frac{\alpha(\alpha-1)\bar{k}^{\alpha-1}}{\sigma(\alpha\bar{k}^{\alpha-1}+1-\delta)} \frac{\bar{c}}{\bar{k}} - 1 \right] & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \end{bmatrix}$$

$$\Gamma_1 = \begin{bmatrix} \alpha\bar{k}^{\alpha-1} + 1 - \delta & -\frac{\bar{c}}{\bar{k}} & 0 & \bar{k}^\alpha & \\ 0 & 0 & 1 & 0 & \\ 0 & 0 & 0 & \left[\frac{\alpha(\alpha-1)\bar{k}^{2\alpha-1} + \rho\alpha\bar{k}^{\alpha-1}}{(\alpha\bar{k}^{\alpha-1}+1-\delta)\sigma} \right] & \rho \\ 0 & 0 & 0 & \rho & \end{bmatrix}$$

$$\Psi = [0, 0, \left[\frac{\alpha(\alpha-1)\bar{k}^{2\alpha-1} + \rho\alpha\bar{k}^{\alpha-1}}{(\alpha\bar{k}^{\alpha-1} + 1 - \delta)\sigma} \right] \sigma_z, \sigma_z]'$$

$$\Pi = [0, 1, 0, 0]'$$

Idea of Perturbation

- Build approximate solutions to economy by starting from
 1. Exact solution of a particular case
 2. Solution of a nearby model whose solution we have access to
- Perturbation algorithms
 1. Taylor series approximation
 2. Around a deterministic steady state
 3. Using implicit-function theorems
- Pros
 1. Accurate around approximation point (in some cases reasonable global performance)
 2. Structure intuitive and easily interpretable
 - e.g. Second-order expansion includes term to correct for volatility of shocks
 3. Traditional linearization \iff First-order perturbation
 4. Dynare makes it accessible

Mathematical Structure

- Recall we wish to solve functional equation

$$\mathcal{H}(d) = \mathbf{0}$$

- If d is an n -differentiable function, apply Taylor's Theorem.
For any $n > 0$...

Theorem

$$d(x) = \sum_{i=0}^{n-1} x^i \frac{d^i(0)}{i!} + \int_0^x \frac{(x-u)^{n-1}}{(n-1)!} d^n(u) du$$

- Without remainder term, we get an approximation with a quantifiable error in a local range i.e. if x is 'near' \bar{x}

$$d(x) \approx d_i(x; \bar{x}) = \sum_{k=0}^i (x - \bar{x})^k \frac{d^k(\bar{x})}{k!}$$

Which Point?

- Generally restrict attention to *Dynamic, Stochastic, General Equilibrium* (DSGE) models
 - Basically (large) set of extensions of stochastic NCG model
 - Includes RBC model, New Keynesian model, BGG Financial accelerator model, etc.
- This class of models usually has a **steady state**
 - A deterministic point in the state space toward which the system converges over time (in the absence of shocks)

Solving the Steady State

- Re-write $\mathcal{H}(d) = 0$ as

$$E_t[\mathcal{H}(y_t, \tilde{y}_{t+1}, x_t, \tilde{x}_{t+1})] = \mathbf{0}$$

- y_t is $n_y \times 1$ vector of controls (choice variables)
- x_t is $n_x \times 1$ vector of states
- $n = n_y + n_x$ number of equilibrium conditions
- Partition states: $x_t = [x'_{1t}; x'_{2t}]'$
 - x_{1t} : $(n_x - n_\epsilon) \times 1$ vector of endogenous states (capital, debt, etc.)
 - x_{2t} : $n_\epsilon \times 1$ vector of exogenous states (productivity, preference shocks, etc.)

Solving the Steady State

- The steady state is defined as a pair of vectors (\bar{x}, \bar{y}) such that

$$\mathcal{H}(\bar{y}, \bar{y}, \bar{x}, \bar{x}) = \mathbf{0}$$

- Solution can often be found analytically
- Not necessarily the same as *stochastic steady state* (\hat{y}, \hat{x})

$$E_t \mathcal{H}(\hat{y}, \hat{y}, \hat{x}, \hat{x}) = \mathbf{0}$$

Stochastic steady state includes response to risk e.g. precautionary saving

Exogenous Process and the Perturbation Parameter

- Exogenous process

$$x_{2,t+1} = \mathbf{C}(x_{2,t}) + \sigma\eta_\epsilon\epsilon'$$

- η_ϵ is covariance matrix
- Generally assume Hessian of \mathbf{C} at \bar{x}_2 has eigenvalues in the unit circle (stationary)
- $\sigma \geq 0$ is the **perturbation parameter**
 - Defines what (exogenous states) we're approximating over
 - Set $\sigma = 0$ at steady state
 - Set $\sigma = 1$ in solution
- Restrict attention to cases in which only shocks are perturbed
 - $\sigma = 0$ implies a deterministic model

Nonlinear Shocks

- Assumption that shocks enter linearly is wlog. If instead

$$x_{2,t} = \mathbf{D}(x_{2,t-1}, \sigma\eta_\epsilon\epsilon_t)$$

- Re-define state to be $\tilde{x}_{2,t} = [x'_{2,t}, \epsilon'_t]'$

- Re-define $x_{2,t} = \tilde{\mathbf{D}}(\tilde{x}_{2,t-1}, \sigma\eta_\epsilon)$

$$\underbrace{\begin{bmatrix} x_{2,t} \\ \epsilon_{t+1} \end{bmatrix}}_{\tilde{x}_{2,t}} = \begin{bmatrix} \tilde{\mathbf{D}}(\tilde{x}_{2,t-1}, \sigma\eta_\epsilon) \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ \epsilon_{t+1} \end{bmatrix}$$

- Can accommodate wide variety of models (stochastic volatility, GARCH, etc.)

Example: Stochastic NCG/RBC Model

- $y_t = c_t$, ($n_y = 1$)
- $x_t = [z_t, k_t]'$, ($n_x = 2$, $n_\epsilon = 1$)
- Function \mathcal{H} written as two equations (replace σ with γ so as not to confuse it with perturbation parameter)

$$(1) \quad c_t^{-\gamma} - \beta(\alpha e^{z_{t+1}} k_{t+1}^{\alpha-1} + 1 - \delta)c_{t+1}^{-\gamma} = 0$$

$$(2) \quad c_t + k_{t+1} - e^{z_t} k_t^\alpha - (1 - \delta)k_t = 0$$

- $x_{2,t} = z_t$. Perturb the shock in the AR(1) process

$$z_{t+1} = \rho z_t + \sigma \eta_\epsilon \epsilon'$$

- Recall steady state sets $\sigma = 0$

Steady State

1. Law of motion implies $\bar{z} = 0$
2. Given this, EE implies

$$\bar{k} = \left(\frac{\alpha}{\rho_{\beta} + \delta} \right)^{\frac{1}{1-\alpha}}$$

where $\rho_{\beta} = 1/\beta - 1$

3. The RC then tells us

$$\bar{c} = \left(\frac{\alpha}{\rho_{\beta} + \delta} \right)^{\frac{\alpha}{1-\alpha}} - \delta \left(\frac{\alpha}{\rho_{\beta} + \delta} \right)^{\frac{1}{1-\alpha}}$$

- Usually a line-by-line procedure can find the steady state
 - Occasionally, a non-linear solver must be used, but problem is generally low dimension

Solution Form

- The (full) solution will be a pair of functions

$$\text{Policy Function: } y = g(x; \sigma)$$

$$\text{Law of Motion: } x' = h(x; \sigma) + \sigma\eta\epsilon'$$

where $g : \mathcal{R}^{n_x} \times \mathcal{R}^+ \rightarrow \mathcal{R}^{n_y}$ and $h : \mathcal{R}^{n_x} \times \mathcal{R}^+ \rightarrow \mathcal{R}^{n_x}$ and

$$\eta = \begin{bmatrix} \emptyset \\ \eta_\epsilon \end{bmatrix}$$

- Define

$$F(x; \sigma) = E_t \mathcal{H}(g(x; \sigma), g(h(x; \sigma) + \sigma\eta\epsilon'; \sigma), x, h(x; \sigma) + \sigma\eta\epsilon')$$

Notice $F : \mathcal{R}^{n_x+1} \rightarrow \mathcal{R}^n$

Perturbing

- Notice that, by definition, $F(x; \sigma) = 0$ for any x and σ
 - Thus, all derivatives of F must be zero as well

$$F_{x_i^k \sigma^j}(x; \sigma) = 0, \quad \forall x, \sigma, i, k, j$$

- Suppose we want a first-order approximation of solution around steady state

$$g(x; \sigma) \approx \bar{y} + g_x(\bar{x}; 0)(x - \bar{x}) + g_\sigma(\bar{x}; 0)\sigma$$

$$h(x; \sigma) \approx \bar{x} + h_x(\bar{x}; 0)(x - \bar{x}) + h_\sigma(\bar{x}; 0)\sigma$$

- Need to find four derivative coefficients; $n \times (n_x + 1)$ distinct terms

Perturbing

- These terms can be pinned down with

$$F_{x_i}(\bar{x}; 0) = 0 \quad \forall i$$

which provides $n \times n_x$ equations, and

$$F_{\sigma}(\bar{x}; 0) = 0$$

which gives n more

- Things are about to get messy...let's prepare...

Tensor Notation

1. A simple way to express loads of terms
 2. Gets rid of \sum and ∂ signs
 3. Points at which derivative is evaluated are also dropped for simplicity
- The derivative of \mathcal{H} with respect to y is an $n \times n_y$ matrix

$$[\mathcal{H}_y]_{\alpha}^i$$

is the i th row and α th column of this matrix

Tensor Notation

- When a sub-index reappears as a superindex in the next term, we are omitting a sum
- For instance, if we want to express how x_j influences y'_i , we use the chain rule to write

$$[\mathcal{H}_y]_{\alpha}^i [\mathcal{G}_x]_{\beta}^{\alpha} [h_x]_j^{\beta} = \sum_{\alpha=1}^{n_y} \sum_{\beta=1}^{n_x} \frac{\partial \mathcal{H}^i}{\partial y^{\alpha}} \frac{\partial g^{\alpha}}{\partial x^{\beta}} \frac{\partial h^{\beta}}{\partial x^j}$$

- For higher derivatives...if we have $[\mathcal{H}_{y'y'}]_{\alpha\gamma}^i$
 - This is a 3-dimensional array with n rows, n_y columns, and n_y pages
 - i th row, α th column, and γ th page

Perturbation Again

- With tensor notation, we can write

$$[F_x(\bar{x}; 0)]_j^i = [\mathcal{H}_{y'}]_\alpha^i [g_x]_\beta^\alpha [h_x]_j^\beta + [\mathcal{H}_y]_\alpha^i [g_x]_j^\alpha + [\mathcal{H}_{x'}]_\beta^i [h_x]_j^\beta + [\mathcal{H}_x]_j^i = \mathbf{0}$$

- There's a lot of these derivatives, but they're all known!
- Notice it's quadratic since we have $g_x h_x$ terms
 - Comes from impact of variables today affecting variables tomorrow through law of motion *and* policy function

Perturbing the Shocks

- Get our last n equations from

$$[F_\sigma(\bar{x}; 0)]^i = E_t \left[[\mathcal{H}_{y'}]_\alpha^i [\mathbf{g}_x]_\beta^\alpha [h_\sigma]^\beta + [\mathcal{H}_{y'}]_\alpha^i [\mathbf{g}_x]_\beta^\alpha [\eta]_\phi^\beta [\epsilon']^\phi + [\mathcal{H}_{y'}]_\alpha^i [\mathbf{g}_\sigma]^\alpha \right. \\ \left. + [\mathcal{H}_y]_\alpha^i [\mathbf{g}_\sigma]^\alpha + [\mathcal{H}_{x'}]_\beta^i [h_\sigma]^\beta + [\mathcal{H}_{x'}]_\beta^i [\eta]_\phi^\beta [\epsilon']^\phi \right]$$

- Since shocks are mean zero and linear, they drop out easily

$$\mathbf{0} = [\mathcal{H}_{y'}]_\alpha^i [\mathbf{g}_x]_\beta^\alpha [h_\sigma]^\beta + [\mathcal{H}_{y'}]_\alpha^i [\mathbf{g}_\sigma]^\alpha + [\mathcal{H}_y]_\alpha^i [\mathbf{g}_\sigma]^\alpha + [\mathcal{H}_{x'}]_\beta^i [h_\sigma]^\beta$$

Certainty Equivalence

- Suppose we have solved the first system for (g_x, g_y, h_x, h_y)
- Plug in with already known \mathcal{H} terms to get that system is
 1. Linear in h_σ, g_σ
 2. Homogeneous in h_σ, g_σ
- Thus, if a unique solution exists, it must be that

$$g_\sigma = 0$$

$$h_\sigma = 0$$

- Solution

$$g(x; \sigma) \approx \bar{y} + g_x(\bar{x}; 0)(x - \bar{x})'$$

$$h(x; \sigma) \approx \bar{x} + h_x(\bar{x}; 0)(x - \bar{x})'$$

Certainty Equivalence

- Solution exhibits **Certainty Equivalence** i.e. first-order approximation identical to first-order approximation of the same model under perfect foresight
- This will *not* be the case for perturbations higher than 1
- Intuitive in context of DSGE model
 - Precautionary motive kicks in when $u'''(\cdot) \neq 0$
 - Euler equation has $u'(\cdot)$, so approximation contains $u''(\cdot)$ terms
 - But no $u'''(\cdot)$ terms!
- Agents respond to *current realizations of shocks*, but take no alternate action *ex ante* because of the presence of shocks

Solving Quadratic Systems

- Square matrix P such that

$$AP^2 - BP - C = 0$$

1. Define two new matrices ($2n \times 2n$)

$$D = \begin{bmatrix} A & \mathbf{0}_n \\ \mathbf{0}_n & I_n \end{bmatrix}, \quad F = \begin{bmatrix} B & C \\ I_n & \mathbf{0}_n \end{bmatrix}$$

2. Find generalized Schur decomposition (QZ) of D and F i.e.

$$Q'\Sigma Z = D$$

$$Q'\Phi Z = F$$

Note: Multiple QZ decompositions based on sorting of diagonals of Σ and Φ

Solving Quadratic Systems

3. Partition Z into

$$Z = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$$

4. Solution is just $P = -Z_{21}^{-1}Z_{22}$

- Multiple QZ decompositions \implies Multiple solutions
- Generally only one will be stable in the eigenvalue < 1 sense
- This will be the one such that $|\phi_{ii}/\sigma_{ii}|$ are in increasing order as we move down the diagonal

Simplifying a Bit

- Quadratic systems can take a while to solve
- Can partition to speed things up a bit
 1. Separate conditions related to $g_x(\bar{x}; 0)$ and $h_x(\bar{x}; 0)$ related to the endogenous state variables
 2. Solve for these (solution exists)
 3. Plug in solution to remaining conditions to get response of exogenous states/stochastic shocks from *linear system*
- Suppose $n_x = 20$, $n_y = 1$, and $n_\epsilon = 5$
 1. All-at-once approach: Quadratic system with 420 unknowns
 2. Partition approach: Quadratic system with 315 unknowns
 - Followed by linear system of 105 unknowns

Our Case

- Our system can be written as

$$F(k_t, z_t; \sigma) = \mathcal{H}(c_t, c_{t+1}, k_t, k_{t+1}, z_t; \sigma) =$$

$$\begin{bmatrix} c(k_t, z_t; \sigma)^{-\gamma} - \beta E_t[(\alpha e^{\rho z_t + \sigma \eta_{t+1}} k(k_t, c_t; \sigma)^{\alpha-1} + 1 - \delta)c(k(k_t, z_t; \sigma), \rho z_t + \sigma \eta_{t+1}; \sigma)^{-\gamma}] \\ c(k_t, z_t; \sigma) + k(k_t, z_t; \sigma) - e^{z_t} k_t^\alpha - (1 - \delta)k_t \end{bmatrix}$$

- Derivatives tell us

$$\mathcal{H}_1 c_k + \mathcal{H}_2 c_k k_k + \mathcal{H}_3 + \mathcal{H}_4 k_k = \mathbf{0}$$

$$\mathcal{H}_1 c_z + \mathcal{H}_2 (c_k k_z + c_k \rho) + \mathcal{H}_4 k_z + \mathcal{H}_5 = \mathbf{0}$$

- Partition system: First row of conditions $\rightarrow (c_k, k_k)$
 - Plug solution into second row $\rightarrow (c_z, k_z)$

Ordering the System

- Gather constant, linear, and higher order terms as follows

$$\begin{bmatrix} 0 & \mathcal{H}_2^1 \\ 0 & \mathcal{H}_2^2 \end{bmatrix} \begin{bmatrix} k_k^2 & 0 \\ c_k k_k & 0 \end{bmatrix} + \begin{bmatrix} \mathcal{H}_4^1 & \mathcal{H}_1^1 \\ \mathcal{H}_4^2 & \mathcal{H}_1^2 \end{bmatrix} \begin{bmatrix} k_k & 0 \\ c_k & 0 \end{bmatrix} + \begin{bmatrix} \mathcal{H}_3^1 & 0 \\ \mathcal{H}_3^2 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

- Rewrite to look quadratic

$$\underbrace{\begin{bmatrix} 0 & \mathcal{H}_2^1 \\ 0 & \mathcal{H}_2^2 \end{bmatrix}}_A \underbrace{\begin{bmatrix} k_k & 0 \\ c_k & 0 \end{bmatrix}^2}_{P^2} + \underbrace{\begin{bmatrix} \mathcal{H}_4^1 & \mathcal{H}_1^1 \\ \mathcal{H}_4^2 & \mathcal{H}_1^2 \end{bmatrix}}_{-B} \underbrace{\begin{bmatrix} k_k & 0 \\ c_k & 0 \end{bmatrix}}_P + \underbrace{\begin{bmatrix} \mathcal{H}_3^1 & 0 \\ \mathcal{H}_3^2 & 0 \end{bmatrix}}_{-C} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

- Column two is filled with zeros...eq'm conditions contained in column one

Our Case

- The \mathcal{H} vectors are as follows

$$\mathcal{H}_1 = \begin{bmatrix} -\gamma \bar{c}^{-\gamma-1} \\ 1 \end{bmatrix}, \quad \mathcal{H}_2 = \begin{bmatrix} \beta(\alpha \bar{k}^{\alpha-1} + 1 - \delta)\gamma \bar{c}^{-\gamma-1} \\ 0 \end{bmatrix}$$

$$\mathcal{H}_3 = \begin{bmatrix} 0 \\ -\alpha \bar{k}^{\alpha-1} - 1 + \delta \end{bmatrix}, \quad \mathcal{H}_4 = \begin{bmatrix} -\beta\alpha(\alpha - 1)\bar{k}^{\alpha-2}\bar{c}^{-\gamma} \\ 1 \end{bmatrix}$$

$$\mathcal{H}_5 = \begin{bmatrix} -\beta\rho\alpha\bar{k}^{\alpha-1}\bar{c}^{-\gamma} \\ -\bar{k}^{\alpha} \end{bmatrix}$$

- Our stable solution ought to feature $k_k < 1$, since

$$k_{t+1} = \bar{k} + k_k(k_t - \bar{k}) + \dots$$

Wrapping things up

- Rest of the system linear

$$\begin{bmatrix} \mathcal{H}_2^1 & \mathcal{H}_1^1 \\ \mathcal{H}_2^2 & \mathcal{H}_1^2 \end{bmatrix} \begin{bmatrix} k_z \\ c_z \end{bmatrix} = - \begin{bmatrix} \mathcal{H}_5^1 + \mathcal{H}_4^1 k_k + \mathcal{H}_2^1 \rho c_k \\ \mathcal{H}_5^2 + \mathcal{H}_4^2 k_k + \mathcal{H}_2^2 \rho c_k \end{bmatrix}$$

- Implies

$$\begin{bmatrix} k_z \\ c_z \end{bmatrix} = - [\mathcal{H}_2 \quad \mathcal{H}_1]^{-1} [\mathcal{H}_5 + \mathcal{H}_4 k_k + \mathcal{H}_2 \rho c_k]$$

- We know that all σ -terms are zero, so we're done!

Comparing Solutions

- Take our first-order solution and manipulate to get in terms of log-differences

$$c_t = \bar{c} + c_k(k_t - \bar{k}) + c_z z_t$$

$$k_{t+1} = \bar{k} + k_k(k_t - \bar{k}) + k_z z_t$$

- Rearrange

$$\hat{c}_t = \frac{\bar{k}}{\bar{c}} c_k \hat{k}_t + \frac{c_z}{\bar{k}} z_t$$

$$\hat{k}_{t+1} = k_k \hat{k}_t + \frac{k_z}{\bar{k}} z_t$$

- Can compare this to our log-linearized, LRE method

Comparing Solutions

- Very different predictions/IRF functions!
- How do we know which one is better?
- Popular method: Euler Equation errors

$$EEE(k_t, z_t) = \left| 1 - \frac{\beta E_t [(\alpha e^{\tilde{z}_{t+1}} k_{t+1}(k_t, z_t)^{\alpha-1} + 1 - \delta) c_t(k_{t+1}(k_t, z_t), \tilde{z}_{t+1})^{-\gamma}]}{c_t(k_t, z_t)^{-\gamma}} \right|$$

1. Simulate model for a long time
2. Compute deviations of approximate solution from true Euler Equations:
3. Average over entire sample
 - Straight average or weighted by ergodic distribution
4. Accuracy Metric: $\log_{10} \bar{EE}$
 - e.g. $-2(-3) \implies$ \$1 mistake for every \$100(\$1000) consumed

A Quick Thought

- Some authors took a different route to simplify
- Kydland and Prescott (1982)
 1. Take second-order approximation of *utility function*
 2. Solve this simpler problem (Linear-Quadratic)
- Also approach taken by Mackowiak and Wiederholdt (2009)
- If all constraints linear, yields same solution as first-order perturbation

Higher-Order

- Natural next step: Up the approximation degree!
- Not clear how to do this when log-linearizing, but straightforward with true perturbation
- Second-order approximation to policy function

$$\begin{aligned} [g(x; \sigma)]^i &= [g(\bar{x}; 0)]^i + [g_x(\bar{x}; 0)]^i_a [(x - \bar{x})]_a + [g_\sigma(\bar{x}; 0)]^i \sigma \\ &\quad + \frac{1}{2} [g_{xx}(\bar{x}; 0)]^i_{ab} [(x - \bar{x})]_a [(x - \bar{x})]_b \\ &\quad + [g_{x\sigma}(\bar{x}; 0)]^i_a [(x - \bar{x})]_a \sigma \\ &\quad + \frac{1}{2} [g_{\sigma\sigma}(\bar{x}; 0)]^i \sigma^2 \end{aligned}$$

- Exactly the same for h

Solving

- Take another derivative of our system $[F_x(\bar{x}; 0)]_j^i$ w.r.t. x (each line is w.r.t. x_k)

$$\begin{aligned}
 0 &= [F_{xx}(\bar{x}; 0)]_{jk}^i = \\
 &\left([\mathcal{H}_{y'y'}]_{\alpha\gamma}^i [g_x]_{\delta}^{\gamma} [h_x]_k^{\delta} + [\mathcal{H}_{y'y'}]_{\alpha\gamma}^i [g_x]_k^{\gamma} + [\mathcal{H}_{y'x'}]_{\alpha\delta}^i [h_x]_k^{\delta} + [\mathcal{H}_{y'x}]_{\alpha k}^i \right) [g_x]_{\beta}^{\alpha} [h_x]_j^{\beta} \\
 &\quad + [\mathcal{H}_{y'}]_{\alpha}^i [g_{xx}]_{\beta\delta}^{\alpha} [h_x]_k^{\delta} [h_x]_j^{\beta} + [\mathcal{H}_{y'}]_{\alpha}^i [g_x]_{\beta}^{\alpha} [h_{xx}]_{jk}^{\beta} \\
 &+ \left([\mathcal{H}_{yy'}]_{\alpha\gamma}^i [g_x]_{\delta}^{\gamma} [h_x]_k^{\delta} + [\mathcal{H}_{yy'}]_{\alpha\gamma}^i [g_x]_k^{\gamma} + [\mathcal{H}_{yx'}]_{\alpha\delta}^i [h_x]_k^{\delta} + [\mathcal{H}_{yx}]_{\alpha k}^i \right) [g_x]_j^{\alpha} + [\mathcal{H}_y]_{\alpha}^i [g_{xx}]_{jk}^{\alpha} \\
 &+ \left([\mathcal{H}_{xy'}]_{\beta\gamma}^i [g_x]_{\delta}^{\gamma} [h_x]_k^{\delta} + [\mathcal{H}_{x'y}]_{\beta\gamma}^i [g_x]_k^{\gamma} + [\mathcal{H}_{x'x'}]_{\beta\delta}^i [h_x]_k^{\delta} + [\mathcal{H}_{x'x}]_{\beta k}^i \right) [h_x]_j^{\beta} + [\mathcal{H}_{x'}]_{\beta}^i [h_{xx}]_{jk}^{\beta} \\
 &\quad + [\mathcal{H}_{xy'}]_{j\gamma}^i [g_x]_{\delta}^{\gamma} [h_x]_k^{\delta} + [\mathcal{H}_{xy}]_{j\gamma}^i [g_x]_k^{\gamma} + [\mathcal{H}_{xx'}]_{j\delta}^i [h_x]_k^{\delta} + [\mathcal{H}_{xx}]_{jk}^i
 \end{aligned}$$

Solving

- Looks complicated, BUT
 - All derivatives of \mathcal{H} are known
 - All first-order terms have already been solved for
- What's left is a series of $n \times n_x \times n_x$ equations in $n \times n_x \times n_x$ unknowns
 - But it's all linear! No quadratic parts anymore!
 - Computer can solve for it easily: Delivers g_{xx} and h_{xx}
- First-order approximation determines whether we are in stable manifold
 - Once we know that, no additional solutions need to be ruled out as we increase the approximation degree

Solving

- Rest of solution can be found separately
- First, note $g_{\sigma x} = h_{\sigma x} = 0$

$$0 = [F_{\sigma x}(\bar{x}; 0)]_j^i =$$

$$[\mathcal{H}_{y'}]_{\alpha}^i [g_x]_{\beta}^{\alpha} [h_{\sigma x}]_j^{\beta} + \mathcal{H}_{y'}]_{\alpha}^i [g_{\sigma x}]_{\gamma}^{\alpha} [h_{\sigma x}]_j^{\gamma} [\mathcal{H}_y]_{\alpha}^i [g_{\sigma x}]_j^{\alpha} + [\mathcal{H}_{x'}]_{\beta}^i [h_{\sigma x}]_j^{\beta}$$

- Cross-partial necessarily zero in unique solution since system is linear and homogeneous

Breaking Certainty Equivalence

- Derivative system for $F_{\sigma\sigma}$ reveals departure from certainty equivalence
- Following system of n equations in n unknowns: $g_{\sigma\sigma}$ and $h_{\sigma\sigma}$
 - Shift constant term in perturbation; precautionary behavior

$$\begin{aligned}
 0 &= [F_{\sigma\sigma}(\bar{x}; 0)]^i = [\mathcal{H}_{y'}]_{\alpha}^i [g_x]_{\beta}^{\alpha} [h_{\sigma\sigma}]^{\beta} \\
 &+ [\mathcal{H}_{y'y'}]_{\alpha\gamma}^i [g_x]_{\delta}^{\gamma} [\eta]_{\xi}^{\delta} [g_x]_{\beta}^{\alpha} [\eta]_{\phi}^{\beta} [I]_{\xi}^{\phi} + [\mathcal{H}_{y'x'}]_{\alpha\delta}^i [\eta]_{\xi}^{\delta} [g_x]_{\beta}^{\alpha} [\eta]_{\phi}^{\beta} [I]_{\xi}^{\phi} \\
 &+ [\mathcal{H}_{y'}]_{\alpha}^i [g_{xx}]_{\beta\delta}^{\alpha} [\eta]_{\xi}^{\delta} [\eta]_{\phi\beta} [I]_{\psi}^{\phi} + [\mathcal{H}_{y'}]_{\alpha}^i [g_{\sigma\sigma}]^{\alpha} \\
 &+ [\mathcal{H}_y]_{\alpha}^i [g_{\sigma\sigma}]^{\alpha} + [\mathcal{H}_{x'}]_{\beta}^i [h_{\sigma\sigma}]^{\beta} \\
 &+ [\mathcal{H}_{x'y'}]_{\beta\gamma}^i [g_x]_{\delta}^{\gamma} [\eta]_{\xi}^{\delta} [\eta]_{\phi}^{\beta} [I]_{\xi}^{\phi} + [\mathcal{H}_{x'x'}]_{\beta\delta}^i [\eta]_{\xi}^{\delta} [\eta]_{\phi}^{\beta} [I]_{\xi}^{\phi}
 \end{aligned}$$

Higher-Order

- As we move up to third, fourth, fifth-order nothing changes
- Each new system is linear given solution of lower-order system
- If computer is autodifferentiating, memory becomes the biggest issue
 - Even very large matrices can be inverted relatively quickly
- We won't solve our benchmark example for second/higher-order yet...
 - Too big to be a useful exercise
 - We'll use Dynare to do it in a bit

Pruning

- Higher-order terms complicate things...
- Linear systems converge globally to their steady state
 - Not true of nonlinear systems!
 - Stable manifold may not span entire relevant space...
- With unbounded shocks (e.g. AR(1)), eventually system will get kicked out of stable region
- Intuition

$$k_{t+1} = a_0 + a_1(k_t - \bar{k}) + a_2(k_t - \bar{k})^2 + \dots + b\epsilon_{t+1}$$

$$k_{t+1} = a_0 + a_1(a_0 + a_1(k_{t-1} - \bar{k}) + a_2(k_{t-1} - \bar{k})^2 + \dots + b\epsilon_t - \bar{k})$$

$$+ a_2(a_0 + a_1(k_{t-1} - \bar{k}) + a_2(k_{t-1} - \bar{k})^2 + \dots + b\epsilon_t - \bar{k})^2 + \dots + b\epsilon_{t+1}$$

Pruning

- Notice k_{t+1} contains k_{t-1} terms raised to the 3rd and 4th powers
- A sufficiently large ϵ_{t-1} shock can push it out of the *radius of convergence*
 - i.e. local space where perturbation is valid
 - Once outside, it will tend to explode as k_{t-1} gets taken to successively higher powers
- Solution: 'Prune' the approximation
 1. Expand 1 period overlap to an n period recursion, where n is the order of the approximation
 2. Get rid of all terms with order (strictly) higher than n i.e. set coefficients to zero
- Pruned system guaranteed not to explode
- Closed-form expression for impulse response functions *and* theoretical moments
 - No need to run simulations to get first and second moments

Perturbing the Value Function

- Sometimes, it is necessary to perturb the value function to solve model
 - Epstein-Zin preferences i.e. recursive utility

$$V(z_t, k_t) = \max_{k_{t+1}, c_t} [(1 - \beta)u(c_t)^\rho + \beta E[V(\tilde{z}_{t+1}, k_{t+1})]^\rho]^\frac{1}{\rho}$$

- Other times, we may want it as a quick (accurate) initial guess for a globally accurate method
- Finally, we may want it to conduct welfare analysis

Perturbing the Value Function

- The value function is treated as a part of the policy function (as opposed to the law of motion)
- The (second-order) perturbed value function is

$$\begin{aligned}V(k_t, z_t; 1) &= \bar{V} + \bar{V}_1(k_t - \bar{k}) + \bar{V}_2 z_t + \frac{1}{2} \bar{V}_{11}(k_t - \bar{k})^2 \\ &\quad + \frac{1}{2} \bar{V}_{22} z_t^2 + \bar{V}_{12}(k_t - \bar{k}) z_t + \frac{1}{2} \bar{V}_{33}\end{aligned}$$

- Easy to prove that $\bar{V}_{33} < 0$. Implies interesting exercise

$$V(\bar{k}, 0; 1) = \bar{V} + \frac{1}{2} \bar{V}_{33} < \bar{V}$$

Perturbing the Value Function

- Can think of $-\frac{1}{2}\bar{V}_{33}$ as the second-order approximation to the welfare cost of business cycles at steady state
 - Relative to perfect foresight economy
- If we wanted to get certainty-equivalent-consumption loss, we need only compute CEC for each case

$$\frac{u(c_{PF})}{1-\beta} = \bar{V} \quad \frac{u(c_{BM})}{1-\beta} = \bar{V} + \frac{1}{2}\bar{V}_{33}$$

- Perfect foresight agent willing to give up to a fraction τ to avoid risk of benchmark business cycles, where

$$(1-\tau)c_{PF} = c_{BM}$$

Solving Higher-Order Perturbations

- Not always ideal to do higher-order perturbations by hand
- Two avenues for mistakes
 1. Derivations by hand
 2. Implementation in code
- Autodifferentiation can get around this
- But others have already done it! Why write it yourself?
 - Dynare: Implementation in Matlab, Octave, Julia, etc.

Dynare

- Dynare is a software platform specifically designed to solve DSGE and OLG models
 - Maintained by Stephane Adjemian, with heavy advice from many leading figures in the field
 - Relatively straightforward interface
1. Enter variables/parameters
 2. Enter equilibrium conditions
 3. Enter steady state (optional)
 4. Define shocks
 5. Select options
 6. Dynare solves model with perturbation

Navigating Dynare: Preamble

- Dynare works in `.mod` files (stands for `'model'`)
 - Comments with `'//'` (`'/*'` comments out sections)
 - End line with `;` (just like Matlab)
 - Objects defined in the preamble
1. `'var'` - Endogenous variables
 2. `'varexo'` - Shocks (not Markov process; literally the shocks)
 3. `'parameters'` - Model parameters
- List parameters first, then initiate line-by-line

Navigating Dynare: Model

- Equilibrium conditions go in 'model' section
- Denote end with 'end;'
- Write expressions with equality (Dynare will automatically set it to zero)
- All variables *assumed* to be denoted at time t e.g. $y_t = y$
 - Denote $t + 1$ variables as $y(+1)$
 - Denote earlier periods as $y(-1)$
 - Larger distances possible

Navigating Dynare: Model Continued

- Note that Dynare will automatically take an expectation over all (+1) variables (no need to specify expectations)
 - Best to denote as period t variables anything *determined* in t
 - e.g. in RBC model, let $k_{t+1} = k$ and $k_t = k(-1)$, since it was determined yesterday
 - Be careful about nested/multiplicative expectations! Often need to define auxiliary variables!
- Dynare will warn you if the number of non-predetermined variables $>$ number of eigenvalues less than one
 - This is called *Blanchard-Kahn* Condition (think back to LRE models for intuition)
 - If not satisfied, solution may not exist or approximation may be unstable/unreliable

Navigating Dynare: Steady State

- Begin with 'initval;'
- End with 'end;'
- Provide steady state values
- Two options
 1. Use exactly what you provided (nothing further)
 2. Use what you provided as an initial guess and solve for SS
 - Follow 'end;' with the 'steady;' command
- If Dynare has trouble finding the steady state, can give it options to use other solvers
- Give command 'check;' after 'steady;' to determine if system is stable (in eigenvalue sense) before we proceed

Navigating Dynare: Shocks

- Start with 'shocks;' command
- Set 'var x = the_variance;' for each shock
- Covariance set by 'var x,y = the_covariance;' for each shock
- End with 'end;'

Solving with Dynare

- When everything in order, end with 'stoch_simul;'
 - Instructs Dynare to solve model with perturbation methods
 - Matlab command: `dynare mydynarecode.mod`
- Delivers
 1. Policy function
 2. Theoretical moments
 3. Variance decomposition
 4. Correlations/autocorrelations
 5. IRFs for all shocks
- Default Taylor order is 2 (automatically prunes)

Solving with Dynare

- Can specify as arguments (among others)
 1. periods = number of simulation periods (default = 0)
 2. order = Taylor approximation order
 3. noprint (ensures nothing printed; may want in a loop)
 4. relative_irf (puts IRF in terms of standard error of shock instead of own % change)
- Dynare puts all results into a Matlab struct (.mat) for later potential use

Example

- Return to stochastic NCG model

$$c_t^{-\sigma} = \beta E_t[(e^{\tilde{z}_{t+1}} \alpha k_{t+1}^{\alpha-1} + 1 - \delta) c_{t+1}^{-\sigma}]$$

$$c_t + k_{t+1} = e^{z_t} k_t^\alpha + (1 - \delta) k_t$$

$$z_t = \rho z_{t-1} + \sigma_z \epsilon_t$$

- Note that $c = c_t$, but $k = k_{t+1}$
- Same parameters as before
- Notice 'correction' term in second-order approximation
 - This is precautionary term, which adjusts the constant
 - Grows as we increase the variance

Example 2

- Nice feature: Can scale up *really* easily
- Consider following model with two shocks (TFP and investment efficiency)

$$\max E_t \sum_{\tau=t}^{\infty} \beta^{\tau-t} \left(\log(c_t) - \theta \frac{h_t^{1+\psi}}{1+\psi} \right)$$

$$c_t + i_t = y_t$$

$$k_{t+1} = e^{b_t} i_t + (1 - \delta) k_t$$

$$y_t = e^{a_t} k_t^\alpha h_t^{1-\alpha}$$

$$\begin{pmatrix} a_t \\ b_t \end{pmatrix} = \begin{pmatrix} \rho & \tau \\ \tau & \rho \end{pmatrix} \begin{pmatrix} a_{t-1} \\ b_{t-1} \end{pmatrix} + \begin{pmatrix} \epsilon_t \\ \nu_t \end{pmatrix}$$

Sidenote: Stationarizing Models

- All of our recursive solution techniques (except for finite-horizon models) assume stationarity
- What if we have a non-stationary model?
 - Sometimes we can solve a transformed, stationarized version
 - Sufficient information is then contained to solve original model
- Most common environment: Growth
 1. Deterministic growth
 2. Stochastic (permanent) growth shocks

Deterministic Growth

- Example: RBC Model with Deterministic Growth
- Production function: $A_t^{1-\alpha} K_t^\alpha$, where

$$A_t = \hat{A}_t e^{z_t}$$

$$\hat{A}_t = e^g \hat{A}_{t-1}$$

for some constant $g > 0$; z_t follows mean-zero AR(1) process

- Normal Bellman equation depends on time

$$V_t(A_t, K_t) = \max_{K_{t+1}} \frac{(A_t^{1-\alpha} K_t^\alpha + (1-\delta)K_t - K_{t+1})^{1-\sigma}}{1-\sigma} +$$

$$\beta E_t \left[V_{t+1}(\tilde{A}_{t+1}, K_{t+1}) \right]$$

i.e. non-stationary

Deterministic Growth

- To solve, define two new objects:

- $\hat{V}_t = V_t(A_t, K_t) / \hat{A}_t^{1-\sigma}$
- $k_t = K_t / \hat{A}_t$

- Can re-write this Bellman as

$$\hat{V}_t(z_t, k_t) = \max_{k_{t+1}} \frac{(e^{(1-\alpha)z_t} k_t^\alpha + (1-\delta)k_t - e^g k_{t+1})^{1-\sigma}}{1-\sigma} + \beta e^{(1-\sigma)g} E_t \left[\hat{V}_{t+1}(\tilde{z}_{t+1}, k_{t+1}) \right]$$

- This Bellman is stationary (can remove the t -subscript)
 - Once solved, can undo transform to get solution to original model

Stochastic Growth

- Same environment, but suppose that

$$A_t = e^{g_t} A_{t-1}$$

and that g_t follows an AR(1) process

- Now, we define

1. $\hat{V}_t = V_t(A_t, K_t)/A_{t-1}^{1-\sigma}$
2. $k_t = K_t/A_{t-1}$

- Transformed system is stationary!

$$\hat{V}_t(g_t, k_t) = \max_{k_{t+1}} \frac{(e^{(1-\alpha)g_t} k_t^\alpha + (1-\delta)k_t - e^{g_t} k_{t+1})^{1-\sigma}}{1-\sigma} + \beta e^{(1-\sigma)g_t} E_t \left[\hat{V}_{t+1}(\tilde{g}_{t+1}, k_{t+1}) \right]$$